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## IMPLEMENTATION OF NEMO-OPA IN CONFIGURATION ORCA-R025

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Centro Euro-Mediterraneo per i Cambiamenti Climatici (CMCC) Istituto Nazionale di Geofisica e Vulcanologia (INGV) masina@bo.ingv.it **SUMMARY** This document describes the NEMO-OPA (Nucleus for European Modelling of the Ocean, Ocean PArallelise) Ocean General Circulation Model (OGCM) in the configuration ORCA-R025 implemented at CMCC. In the first part it gives a description of the most important technical aspects of the model, the physical parameterization adopted and the forcing used.

In the second part, the results of the benchmarks on the vector and scalar systems of the CMCC Computer Center are presented and compared.

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This report describes the implementation of ORCA-R025 at the Numerical Applications and Scenarios Division of CMCC. The ORCA-R025 implemented at CMCC is a global 1/4° configuration of NEMO-OPA ocean circulation model (Madec, 2008) [6] and the code is based on version NEMO 2.3. The model has been implemented on three different supercomputers available at CMCC:

- A vector system of 4 nodes for a total of 30 NEC SX-8R processors (3 nodes equipped with 8 CPUs and 1 node with 6 CPUs) located at CIRA in Capua with a peak performance of 1 TFlops.
- A vector system of 112 NEC SX-9 processors distributed on 7 nodes with a peak performance of 11,47 TFlops situated inside the Campus "Ecotekne" in Lecce.
- A scalar system of 30 nodes for a total of 960 IBM Power 6 CPUs with a peak performance of 18 TFlops situated inside the Campus "Ecotekne" in Lecce.

A first benchmark of the code has been carried out on the cluster of NEC SX-8R in order to find the best choice of the domain decomposition. Afterward, the code has been imported on the cluster of NEC SX-9 and the benchmark of the code has been done again by varying the number of CPUs while keeping the same best domain decomposition found on the vector system located in Capua.

An additional benchmark has been carried out to asses the performance of the code on the cluster of IBM Power 6 processors.

All the simulations have been done without the ice model and with the same forcing dataset. It consists of the climatological year derived by the ENACT dataset (Bellucci et al., 2007)

[2] More details will be given in section *ENACT Dataset* .

#### **BASIC SETTINGS**

The list of the CPP keys used for the simulations in configuration ORCA-R025 is found in table 1

#### Table 1 CPP keys for ORCA-R025

(		
ORCA-R025	Description	
key_		
orca_r025	Configuration name	
dynspg_flt	Filtered free surface	
zdftke	TKE vertical mixing scheme	
zdfddm	Double diffusive mixing	
zrefsurf	Increment of the vertical back-	
	ground eddy viscosity for dy-	
	namic and vertical background	
	eddy diffusivity for tracers near	
	the surface (former 10 layers)	
	and uses a different vertical layer	
	distribution	
dtatem	Use temperature data for initial	
	conditions	
dtasal	Use salinity data for initial condi-	
	tions	
dtasst	Use sea surface temperature	
	data for damping	
traldf_c2d	2D lateral diffusion for tracers	
	(depends on $\delta x$ )	
lim_fdd	Sea/Ice interaction	
dynldf_c3d	3D lateral diffusion for dynamics	
	(depends on $\delta x^3$ )	
ldfslp	Need to calculate isopycnal	
	slope	
trabbl_dif	Diffusive bottom boundary layer	
	parameterization	
trabbc	iracer bottom boundary condi-	
	tion Deutic Lead tage annuality	
partial_steps	Partial cell topography	
tau_dally	Establishes that the stress is up-	
	Catebliebes that the fluxes are	
lix_lorced_dally	undeted every dev	
diagan	Model data gan diagnostic	
diahth	Thermocline diagnostic	
dynhpa	Hydrostatic pressure anomaly	
ayimpa	diagnostic	
iam aam	Parallelization through MPI	
vectopt_loop	Computational optimization on	
T T T T T T T T T T T T T T T T T T T	vector machines	
vectopt_memorv	Memory optimization for vector	
	machines	

#### **HORIZONTAL GRID**

The horizontal grid (Fig. 1) has 3 poles (2 poles in the northern hemisphere, one over Canada and the other over Siberia). The horizontal grid resolution is 1/4 deg at the equator for both latitude and longitude, leading to horizontal dimensions of 1442 X 1021. The minima of the scale factors (ocean points) are around 5.6 Km (zonal direction) and 3.2 Km (meridional direction). The maximum is 27.8 Km at the equator.



In Fig. 1, the closed sea are not present because we are running without them. This option may be set in the namelist as follows:

```
!-----
!...
! nclosea = 0 no closed sea
! = 1 closed sea (Black
Sea, Caspian Sea, Great US
Lakes...) 5760
!...
nclosea = 0
```

#### **VERTICAL GRID**

There are 50 levels on the vertical, with a grid spacing depending on the key\_zrefsurf CPP key. If the key is used, the grid spacing ranges from 1 m near the surface to 450 m at 5750 m. In the other case, the grid spacing ranges from 6 m near the surface to 450 at 6000 m. Figure 2 compares the vertical distribution of the layers between the two configuration of ORCA-R025 (with and without key\_zrefsurf) and a version of the OPA 8.2 in configuration ORCA2 also used at CMCC (Di Pietro et al.) [3] (Scoccimarro et al., 2007) [10].

It is important to stress here that the vertical spacing of ORCA2 configuration is more resolved than ORCA-R025 at depths between 50 m and 200 m when the key\_zrefsurf is used.



#### BATHYMETRY

The bathymetry file has been constructed and provided by MERCATOR OCEAN. It is derived from two input files:

- The 2-minute bathymetry file (etopo2) of NGDC, combination of (Smith & Sandwell, 1997) [11] satellite-based bathymetry (8.2 version), IBCAO (in the Arctic region) and other data in the Antarctic region. The MERCATOR project team has applied additional corrections near the Antarctic (Remy et al., 2003) [9]. This file is used for the deep ocean (below 300m).
- The GEBCO 1mn bathymetry file provided between 88S and 88N. This file is used for bathymetry on the shelf because it is found to be more accurate there (above 200m).

#### **INITIAL CONDITIONS**

The initial conditions for temperature and salinity were derived from the Levitus98 (Levitus S. et al, 1998) [5] data set. The zonal and the meridional components of the velocity field start from zero value.

#### FORCINGS

#### **RUN-OFFS**

The runoff file has been provided by MERCATOR-OCEAN. It includes 99 major rivers and coastal runoffs. It is a monthly climatology.

The namelist variable nrunoff=2 has been set. In that case, a special treatment is applied in runoff regions, where the array *upsrnfh* is non zero. This array is read in the runoff file (netcdf variable *socoefr*). It has a value of zero where there is no runoff and 0.5 at runoff points. Since the centered scheme has not been used, there is no need to revert to upstream near runoffs (see Section *Numerical schemes*). The special treatment consists in an enhanced vertical diffusion at the interface of layers 1 and 2 applied in step.F90: avt (:,:,2) = avt (:,:,2) + 2.e-3 \* upsrnfh (:,:)

The vertical mixing is then set to  $10^{-3}$  below the top level at runoff points.

*upsrnfh* is also used to avoid SSS restoring in the vicinity of river mouths.

#### **ENACT DATASET**

The wind stress, solar heat flux, absorbed solar radiation and evaporation minus precipitation fields come from the ENACT data set. The available fields are all daily mean values and therefore they cannot represent the diurnal cycle. They are derived from 0-24 hour averages from the ERA-40 (Uppala et al., 2005) [13] reanalyses. The main difference between the ERA-40 data set and the ENACT data set concerns the precipitation field which has been corrected for a bias (Troccoli & Källberg, 2004) [12].

The model has been forced with a climatological year (1958-2001) with daily values.

The original ENACT data set at the resolution of T106, i.e., the full resolution of ERA-40 has been interpolated onto the ORCA-R025 horizontal grid and rotated to take into account its distortion north of 40<sup>0</sup> N. The OASIS3 package (Valcke, 2006) [14] with a simple bilinear interpolation has been used.

#### SEA SURFACE HEIGHT ADJUSTMENT

A SSH adjustment has been used in order to take into account the fact that the fresh water budget, i.e., E-P-R is not close and can be the cause of a spourious drift of the SSH. ln\_fwb = .true. has been set in the namelist. The code has been modified to allow a daily adjustment instead of a yearly one.

#### SURFACE RELAXATION

SST has been relaxed to the ERA-40 SST with a restoring time of 12 days corresponding to a

damping term of 200  $W/m^2/C$  in the heat flux. No relaxation has been applied either to SSS or T and S on the whole water column.

#### PARAMETRIZATIONS

All runs are performed with the free surface, constant volume formulation (key\_dynspg\_flt defined).

#### LATERAL MIXING

A laplacian isopycnal diffusion scheme is used for tracers with  $aht0=300m^2/s$  at the equator. The coefficient decreases poleward proportionally to the grid size. Associated keys are traldf\_c2d and ldfslp.

A biharmonic horizontal viscosity is used for dynamics with  $ahm0=-1.5 \ 10^{11} \ m^4/s$ . The viscosity depends on the grid size at the cubic power according to the equation 1

$$ahm = ahm0 * \frac{\delta x^3}{\delta x_{max}^3} \tag{1}$$

#### **VERTICAL MIXING**

There is double-diffusive mixing zdfddm. Turbulent Kinetic Energy scheme is used to compute the vertical mixing zdftke with the following namelist parameters

```
! ------
! namtke turbulent eddy kinetic
dependent vertical diffusion
! ( #ifdef "key_zdftke" )
!------
! ln_rstke flag to restart
with tke from a run without tke
(default F)
! ediff coef. to compute vertical
eddy coef. (avt=ediff*mxl*sqrt(e)
```

```
)
! ediss coef. of the Kolmogoroff
dissipation
! ebb coef. of the surface input
of tke
  efave coef. to applied to the
!
tke diffusion ( avtke=efave*avm )
! emin minimum value of tke
(m^2/s^2)
! emin0 surface minimum value of
tke (m^2/s^2)
! nitke number of restart
iterative loops
! ri_c critic richardson number
! nmxl flag on mixing length used
! = 0 bounded by the distance to
surface and bottom
! = 1 bounded by the local
vertical scale factor
! = 2 first vertical derivative
of mixing length bounded by 1
! npdl flag on prandtl number
! = 0 no vertical prandtl number
(avt=avm)
! = 1 prandtl number function of
richarson number (avt=pdl*avm)
! = 2 same as = 1 but a shapiro
filter is applied on pdl
! nave = horizontal averaged
(=1/2) or not (=0) of avt (default
=1)
!&namtke
ln_rstke = .false.
ediff = 0.1
ediss = 0.7
ebb = 60.
efave = 1.
emin = 1.e-6
emin0 = 1.e-4
nitke = 50
nmxl = 2
npdl = 1
navb = 0
```



nave = 1

The enhanced vertical diffusion is used when convection is diagnosed. The corresponding namelist block is:

#### BOTTOM FRICTION AND LATERAL BOUNDARY CONDITION

The namelist for the bottom friction is the following.

|\_\_\_\_\_

```
1_____
! namzdf vertical physics
|_____
!
 ln_zdfevd enhanced vertical
diffusion (default T)
! ln_zdfnpc Non-Penetrative
Convection (default T)
! avm0 vertical eddy viscosity for
the dynamic (m^2/s)
! avt0 vertical eddy diffusivity
for tracers (m^2/s)
! avevd vertical coefficient for
enhanced diffusion scheme (m^2/s)
! nevdm = 0 apply enhanced mixing
on tracer only
! = 1 apply enhanced mixing on
both tracer and momentum
! ln_zdfexp vertical physics:
(=T) time splitting (T)
(Default=F)
! (=F) euler backward (F)
! n_zdfexp number of sub-timestep
for time splitting scheme
&namzdf
ln_zdfevd = .true.
ln_zdfnpc = .false.
avm0 = 1.e-4
avt0 = 1.e-5
avevd = 10.
nevdm = 1
ln_zdfexp = .false.
n_zdfexp = 3
```

ļ nambfr bottom friction |\_\_\_\_\_ nbotfr type of bottom friction 1 ! nbotfr = 0 , no slip nbotfr = 1 , linear friction ! ! nbotfr = 2 , nonlinear friction ! nbotfr = 3 , free slip ! bfril bottom drag coefficient (linear case) ! bfri2 bottom drag coefficient (non linear case) ! bfeb2 bottom turbulent kinetic energy  $(m^2/s^2)$ ! ln\_bfr2d: flag for 2d coef enhancement read in file ! bfrien: enhancement coefficient (integer > 1) ! bfrien = 30 ! ln\_bfr2d = .TRUE. &nambfr nbotfr = 2bfri1 = 4.e-4bfri2 = 1.e-3bfeb2 = 2.5e-3

A diffusive bottom boundary layer is activated using trabbl\_dif with atrbbl=3000  $m^2/s$ .

The lateral boundary conditions can be set to *no-slip*, *free-slip*, *partial free-slip* or *strong no-slip*. The namelist parameter to be set is shlat. For more details, please refer to (Madec, 2008) [6].

The free slip condition has been previously

used but it gives strong currents in the Indonesian Through-Flow (ITF) straits. Therefore we decided to set the no slip lateral boundary condition. Fig 3 shows the transport of mass in the Lombok strait for two experiments which differ just for the lateral boundary conditions. The experiment with no-slip lateral condition is much more consistent with experimental observed data. In fact, the average value is 2.3 Sv which is close to the value of 1.7 Sv stated by (Murray & Arief., 1988) [7] while the free-slip condition experiment gives an average of 6 Sv.



In the Technical report (Dussin et al., 2009) [8] they use the free slip condition because in a previous simulation with the no slip condition they were not satisfied about the results. However, they indicate that with the free slip condition the transports in the ITF are too strong so they modified the condition locally in order to decrease them. At the light of our initial results and the results reported in Dussin et al., (2009) a final decision on the best lateral conditions to be used with the present version of ORCA-R025 is therefore still under evaluation.

#### NUMERICAL SCHEMES

#### **ADVECTION SCHEMES**

The Total Variance Dissipation (TVD) scheme for tracers is used (ln\_traadv\_tvd=.true.) together with the energy enstrophy advection scheme suitable for partial step topography (ln\_dynvor\_een=.true.).

The other possible advection schemes for tracers are the  $2^{nd} \ {\rm order} \ {\rm centred} \ {\rm scheme}$ 

(ln\_traadv\_cen2=.true.), the Monotone Upstream Scheme for Conservative Laws (MUSCL)

(ln\_traadv\_muscl=.true.)

and a second MUSCL scheme (ln\_traadv\_muscl2=.true.).

The other possible advection scheme for dynamics are the enstrophy conserving scheme (ln\_dynvor\_ens=.true.), the energy conserving scheme (ln\_dynvor\_ene=.true.) and the mixed scheme (ln\_dynvor\_mix=.true.).

The reader interested in more details can refer to the manual of NEMO (Madec 2008) [6].

#### TIME DISCRETIZATION

The model uses a Leapfrog scheme for nondiffusive processes with an Asselin (Asselin, 1972) [1] time filter with the Asselin coefficient set to 0.1. For the non- diffusive part, two different schemes are available: a) a forward time differencing scheme using a time splitting technique (ln\_zdfexp=.true. in the namelist) or b) a backward time differencing scheme (ln\_zdfexp=.false.). Here, we use the second option. The time step is set to 1080 s (80 steps/day).



#### **MODEL OUTPUT**

#### **ARCHIVED FIELDS**

Files are stored every 5 days (nwrite = 300 steps) with 5 days averaged fields. 3D variables are

- vozocrtx Zonal velocity (in grid\_U.nc)
- vomecrty Meridional velocity (in grid\_V.nc)
- votemper Temperature (in grid\_T.nc)
- vosaline Salinity (in grid\_T.nc)
- vovecrtz Vertical velocity (in grid\_W.nc)
- votkeavm Vertical eddy viscosity (in grid\_W.nc)
- votkeavt Vertical eddy diffusivity (in grid\_W.nc)
- votkeevm Enhanced vertical viscosity
  (in grid\_W.nc)
- votkeevd Enhanced vertical diffusivity (in grid\_W.nc)
- voddmavs Salt vertical eddy diffusivity (in grid\_W.nc)

Two dimensional fields are sozotaux (zonal wind stress), sozotauy (meridional wind stress) and soleahtw (lateral eddy diffusivity) (in grid\_U, grid\_V and grid\_W files respectively), and in grid\_T files:

- sossheig Sea surface height (meters)
- somx1010 Mixed layer depth (meters) based on a  $\sigma_0$  difference of 0.01 with the surface

- sohefldo Net downward heat flux (Wm<sup>-2</sup>)
- soshfldo Short wave downward radiative flux (Wm<sup>-2</sup>)
- sowaflup Net upward water flux (Kg m<sup>-2</sup>s<sup>-1</sup>)
- sosstsst Sea surface temperature (K)
- sosaline Sea surface salinity (PSU)
- sorunoff Runoffs (Kg m<sup>2</sup>s<sup>-1</sup>)
- sowaflcd Concentration/Diluition water
  flux (Kg m<sup>-2</sup>s<sup>-1</sup>)
- sosalflx Surface salt flux (Kg m<sup>-2</sup>s<sup>-1</sup>)
- somixhgt Turbocline depth (meters)
- soicecov lce cover [0,1]
- sohefldp Surface heat flux damping (Wm<sup>-2</sup>)
- sowafldp Surface water flux damping (Kg  $m^{-2}s^{-1}$ )
- sosafldp Surface salt flux damping (Kg m<sup>-2</sup>s<sup>-1</sup>)
- sobowlin Bowlindex
- sothedep Thermocline depth (m)
- so20chgt Depth of 20C isotherm (m)
- so28chgt Depth of 28C isotherm (m)
- sohtc300 Heat content 300 m (W)
- sohpa Hydrostatic pressure anomaly (m)



STORAGE

The output is written by each processor in direct access files. All these partial files are merged by means of the flio\_rbld tool provided by IOIPSL. The outputs are netcdf files written for each month and the filenames are of kind ORCA025\_spinup\_5d\_yyyymm01\_yyyymmld \_grid\_X.nc, where 5d says that the output is stored every 5 days, yyyy is the year, mm is the month, ld is the last day of the month and x stands for T, U, V or W. All files are stored in ans007@ulysses.cmcc.it.

#### **CODE STRUCTURE**

#### **COMPILING ENVIRONMENT**

The NEMO code is located under the directory .../nemo025. Table 2 shows the directory tree of NEMO.

The code is designed to run on the NEC-SX8R/9 vector supercomputer and on massive parallel machines.

In order to compile the code, the following prerequisite are needed:

- the MPI library
- the NetCDF library
- the GNU make

According to the NEC supercomputer, the compilation of the code can be done using the NEC cross-compiler on a front-end machine.

#### **RUNNING ENVIRONMENT**

The running environment is divided in two sections:

- experiment management (../nemo025/ config/ORCA025\_LIM/EXPID)
- experiment directory tree (../EXPID)



where EXPID is the name of the generic experiment.

Note that the experiment management directory tree ../nemo025/config/ORCA025\_LIM/EXPID is located in the ../nemo025 main directory and that the EXPID subdirectories need to be created for every new experiment. The ../EXPID directory is usually placed on a fast filesystem.

The shell script JOB\_recur, located in the .../nemo025/config/ORCA025\_LIM/EXPID directory, is the one used to run the experiment. The script needs to have specified the environment variables of the experiment to be run.

A chain submission procedure is applied to avoid too long jobs on the computing platform. In our current configuration, the model is designed to run 1 month of simulation for each job submission. The information regarding the month to integrate after the first submission is stored in a text file named time.txt which is generated by the JOB\_recur script during the first submission. The time.txt file contains year and month in execution.

The JOB\_recur script is submitted to the NEC-SX NQS (IBM lsf) batch system through the qsub (bsub) command and executes the following steps:

- 1. Set the environment variable related to:
  - experiment name
  - paths of the directory tree
  - number of processes to be used
- Modify the namelist according to the job to run
- Get the executables, the namelist and create the links to the forcings and the restart files in the scratch directory where the job will run
- 4. Launch the job
- 5. Save the output and the restart files in the storage directory
- 6. Update the time.txt file
- 7. Resubmit itself to perform the next month (until the end of the experiment)

#### **NUMERICS**

#### **DOMAIN DECOMPOSITION**

A different domain decomposition has been chosen for the two available supercomputer architectures. The criterion that drives this choice is a compromise between the efficiency of the code and the available computing resources. The available computing resources refer not only to the potential of the machine but also to the requests of all the users which access the supercomputer. Our best choice is therefore a domain decomposition of 8 zonal domain for the vector system while for the scalar system there is not any particular choice because as it will be shown in Section *Benchmark on scalar system*, the efficiency of the code is almost the same for a number of CPUs greater than 25.

Section *Benchmark on vector system* describes the benchmarks done on the cluster of SX-8R and on the cluster of SX-9.

Section *Benchmark on scalar system* describes the benchmark on the scalar system. In this case we did not assess the most performant domain decomposition, given a number of available CPUs. This kind of analysis would have requested an exaggerate CPU time with respect to the benefits that could have been derived.

#### **BENCHMARK ON VECTOR SYSTEM**

### BRIEF DESCRIPTION OF THE VECTOR SYSTEM

Two different benchmarks of the code have been carried out, respectively on the cluster of NEC SX-8R and on the cluster of NEC SX-9. The vector system located at CIRA consists of 4 nodes for a total of 30 NEC SX-8R vector CPUs (3 nodes equipped with 8 CPUs and 1 node with 6 CPUs) and a peak performance of 1 TFlop. Here we assessed the most convenient geometry for the domain decomposition and afterward we made another benchmark on the cluster of SX-9 just varying the number of CPUs while keeping the most convenient geometry. The vector system located at Ecotekne consists of 112 NEC SX-9 vector CPUs for a total peak performance of 11.47 TFlop.

#### **DESCRIPTION OF THE SIMULATION**

The simulations done on the cluster of SX-8R and on the cluster of SX-9 in order to asses the performance of the code have a duration of one month. The forcing used and the physical parametrizations are identical to what has been

largely described in the section Forcings .

#### PERFORMANCE

A first analysis of the performance has been conducted on the cluster NEC SX8-R. In order to do that, a series of runs have been made with a different number of CPUs ranging from 4 to 16 by evaluating the efficiency of the code. The domain decomposition used in these runs is of the kind 2XY where 2 is the number of domain along the zonal direction and Y is along the meridional direction. For example, a domain decomposition 2X8 means 2 meridional domains and 8 zonal domains.

Figures 4, 5 and 6 show respectively the user and the elapsed time for all the simulations on the cluster of SX-8R, the speed-up with respect to the simulation with domain decomposition 2 X 2 and the efficiency with respect to the same domain decomposition. The first thing to note is that the code loses lots of efficiency when using 8 CPU. It seems that this domain decomposition is particularly disadvantageous. We investigated on the possible causes of this result and we found that the code produces a high bank conflict time when employing 8 CPUs. This time doubles with respect to the other simulations, but it does not depend on the particular domain decomposition. In fact, figure 7 shows that elapsed and user time of the simulations performed with all possible domain decompositions with 8 CPUs do not vary in a significant way. Anyway, this trend is not found on the cluster NEC SX9 (figure 10). More experiments should be done to investigate on the possible causes.

All the possible combinations of domain decomposition with 8 CPUs were tested and as figure 7 shows, the simulations with domain decomposition  $1 \times 8$  is most performant if we consider the elapsed time while is equivalent to domain decompositions  $2 \times 4$  and  $4 \times 2$  if we consider





#### the user time.

Figures 8, 9 and 10 show respectively the elapsed and the user time for all the simulations, the speed-up with respect to the simulation with domain decomposition 1 X 4 and the efficiency with respect to the same domain decomposition on the cluster of NEC SX9.

Figures 9 and 10 show that the code loses lots of efficiency when using more than 8 CPUs. In particular, the efficiency (with respect to 4 CPUs) dumps to 70% (if we consider the user time and 50% if we consider the elapsed time) when employing 16 CPUs while it is 90% for 8





CPUs. Therefore, 8 CPUs seems to be the best compromise between the efficiency of the code and the availability of the computing resources. The last consideration is referred to the NEC SX-8R and SX-9 CPUs. The peak performance of one CPU is 35.2 GF and 102.4 GF respectively, so the speed-up should be around 2.9, when moving from SX-8R to SX-9. Table 3 shows the elapsed time and the user time for the simulation with domain decomposition 1 X 4 on both clusters, and the speed-up between of them.





Table 3Performance comparison between the clusters SX-8Rand SX-9 for the domain decompsition 1 X 4		
	elapsed (s)	user (s)
SX-8R	9761.1	9324
SX-9	3845.9	3220.6
speed up	2.53	2.89

Table 3 shows that the real speed-up is similar

to what expected.



#### **BENCHMARK ON SCALAR SYSTEM**

### BRIEF DESCRIPTION OF THE SCALAR SYSTEM

The scalar system on which the benchmark has been carried out is located at Campus "Ecotekne" in Lecce. It consists of 960 IBM Power 6 CPUs distributed on 30 multicore nodes, for a total peak performance of 18 TFlops.

#### **DESCRIPTION OF THE SIMULATION**

The simulation done to assess the performance of the code has a duration of one month. The forcing used for this simulation and the physical parametrizations are identical to what has been largely described in the section *Forcings*.

#### PERFORMANCE

A different strategy for the domain decomposition has been adopted for the benchmark on the scalar system with respect to the vector system case. In the other case, we choose to evaluate the performance for a domain decomposition of the kind 2 X Y where 2 is the number of domain along the zonal direction and Y is along the

meridional direction. In this case we adopted a domain decomposition of the kind N X N where N varies between 2 and 13. It could be simpler to asses the performance for a domain decomposition for a multiple of 4 or 16 or 32 and have a linear axis for the number of CPUs employed. However, we thought that two different performances are better comparable if the geometry of their domain decomposition is similar. In the scalar system case we had much more available CPUs with respect to the vector system case and this was possible. Figures 11, 12 and 13 show respectively the elapsed and the user time for all the simulations, the speed-up with respect to the simulation with domain decomposition 2 X 2 and the efficiency with respect to the same domain decomposition.



Figures 12 and 13 show that the code loses dramatically efficiency when using more than 16 CPUs and stabilizes on 50% if we consider the elapsed time or the 60% if we consider the user time. Running with less than 64 CPUs is not workable because this would imply more than 5 hours (the time required when 64 CPUs are used) per month of simulation, so, we have to consider that, for practical use, the code has an efficiency of about 50%.

As said before, we did not investigate the best





geometry for the domain decomposition. This analysis would make sense for a large number of CPUs which is plausible for a realistic operational use. On the other hand, this would request a strong effort in terms of CPU time considering the large number of combination of different domain decomposition for a number of order 100.

#### Input files: Grid coordicoordinates\_ORCA025\_LIM.nc nate file bathy\_ORCA025\_LIM.nc Ocean bathymetry file EMPave\_old.dat Initial Average EMP Levitus98\_PHC21\_Sal\_ORCA\_R025.nc Salinity climatology from Levitus (Levitus98\_Sal\_nodirect.nc) Levitus98\_PHC21\_Tem\_ORCA\_R025.nc Potential Temperature climatology from Levitus (Levitus98\_Tem\_nodirect.nc) runoff\_ORCA025\_LIM.nc Climatological run-off Gr\_SST\_clim\_58\_01.nc ERA-40 SST

### **RESTART FILES**

Restart file:	
ORCA025_EXPID_YYYYMMDD_restart.nc	Restart
	file

### **OUTPUT FILES**

Output files:	ORCA025 EXPID 5d	VYYYMMID VYYYMMED
Output mes.	OKCHOZJ_BALID_JC	

grid_T	Output frequency:
	monthly; Format: NetCDF
grid_U.nc	Output frequency:
	monthly; Format: NetCDF
grid_V.nc	Output frequency:
	monthly; Format: NetCDF
grid_W.nc	Output frequency:
	monthly; Format: NetCDF

#### **AUXILIARY FILES**

#### **INITIAL AND BOUNDARY CONDITIONS**

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